

EAS6939 Homework #6

1. In engineering, the random wind pressure (Y) is typically modeled as a quadratic transformation of the random wind speed (X). If $X \sim N(\mu_x, \sigma_x^2)$ and $Y = X^2$, find approximation of Y based on the first-order Taylor series expansion about mean of X and equivalent linearization. For equivalent linearization, consider $Y_L = aX + b$, where a and b are optimal parameters. Calculate the mean and variance of the above approximations of Y .

Solution:

1) First-order Taylor series expansion:

$$Y_L = Y(\mu_x) + \left. \frac{dY}{dX} \right|_{x=\mu_x} (X - \mu_x) = 2\mu_x X - \mu_x^2$$

Therefore, the approximate mean and variance are

$$\mu_Y = E[Y_L] = 2\mu_x E[X] - \mu_x^2 = \mu_x^2$$

$$\sigma_Y^2 = (2\mu_x)^2 \text{Var}[X] = 2\mu_x^2 \sigma_x^2$$

2) Equivalent linearization:

The model parameters a and b can be obtained from:

$$\underset{a,b}{\text{minimize}} E[Y_L - Y]^2$$

For a general case, the minimizing conditions become

$$aE[X^2] + bE[X] = E[X^3]$$

$$aE[X] + b = E[X^2]$$

From class,

$$E[X^2] = \sigma_x^2 + \mu_x^2$$

$$E[X^3] = 2\mu_x \sigma_x^2 + \mu_x^3$$

Therefore, parameters a and b are calculated by

$$a = 2\mu_x \quad b = \sigma_x^2 - \mu_x^2$$

And the linearized equation becomes

$$Y_L = 2\mu_x X + \sigma_x^2 - \mu_x^2$$

And the mean and variance become

$$\mu_Y = \sigma_x^2 + \mu_x^2$$

$$\sigma_Y^2 = 4\mu_x^2 \sigma_x^2$$

2. A vehicle has a deterministic mass, $m = 2$, and random velocity, V , which can take on both positive and negative values. The kinetic energy (K) of the vehicle is $K = \frac{1}{2}mV^2$. If V follows Normal (Gaussian) probability distribution with mean, $m_V = 0$, and standard deviation, $\sigma_V = 1$, determine the probability density function and cumulative probability distribution function of K . Use the method of general transformation.

Solution:

Since the relationship, $K = V^2$, is nonlinear, the method of general transformation needs to be used.

CDF of K :

$$\begin{aligned}
 F_K(k) &= P(K \leq k) \\
 &= P(V^2 \leq k) \\
 &= \int_{R=\{V^2 \leq k\}} f_V(v) dv \\
 &= 2 \int_{-\sqrt{k}}^{\sqrt{k}} \frac{1}{\sqrt{2\pi}} \exp\left(-\frac{1}{2}v^2\right) dv \\
 &= 2 \left[\frac{1}{2} - F_V(-\sqrt{k}) \right] \\
 &= 1 - 2F_V(-\sqrt{k}) \quad \text{for } k \geq 0
 \end{aligned}$$

Since V is Normal with zero mean, $F_V(-v) = 1 - F_V(v)$ for any v . Hence, the CDF of K can be written as

$$F_K(k) = 2F_V(\sqrt{k}) - 1 = F_V(\sqrt{k}) - F_V(-\sqrt{k})$$

Since K is always positive, the complete PDF of K is

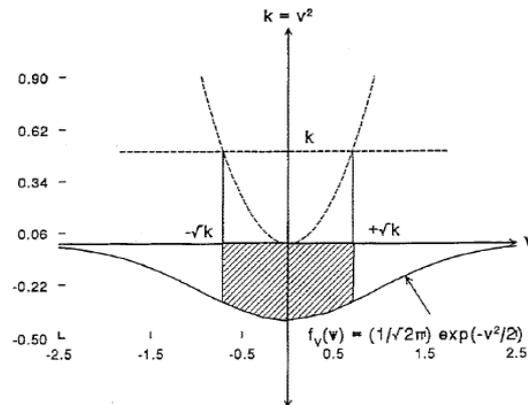
$$f_K(k) = \begin{cases} 0 & k < 0 \\ F_V(\sqrt{k}) - F_V(-\sqrt{k}) & k \geq 0 \end{cases}$$

PDF of K :

By differentiating PDF of K ,

$$\begin{aligned}
 f_K(k) &= \frac{dF_K(k)}{dk} = 2 \frac{dF_V(\sqrt{k})}{dk} \\
 &= 2f_V(\sqrt{k}) \frac{1}{2} \frac{1}{\sqrt{k}} \\
 &= \frac{1}{\sqrt{2\pi k}} \exp\left(-\frac{1}{2}k\right), \quad k \geq 0
 \end{aligned}$$

This is one-degree-of-freedom chi-square probability.



3. The resistance (or strength), R , of a mechanical component which is subject to a load, S , are modeled as random variables with the following probability density function:

$$f_R(r) = \begin{cases} 0.5 & 0 \leq r \leq 2 \\ 0 & \text{otherwise} \end{cases} \quad f_S(s) = \begin{cases} 2s & 0 \leq s \leq 1 \\ 0 & \text{otherwise} \end{cases}$$

Assume that R and S are statistically independent. Find the cumulative probability distribution functions, $F_Y(y)$ and $F_Z(z)$ of

(a) $Y = R - S$

(b) $Z = R/S$

Furthermore, evaluate

(c) $F_Y(0)$

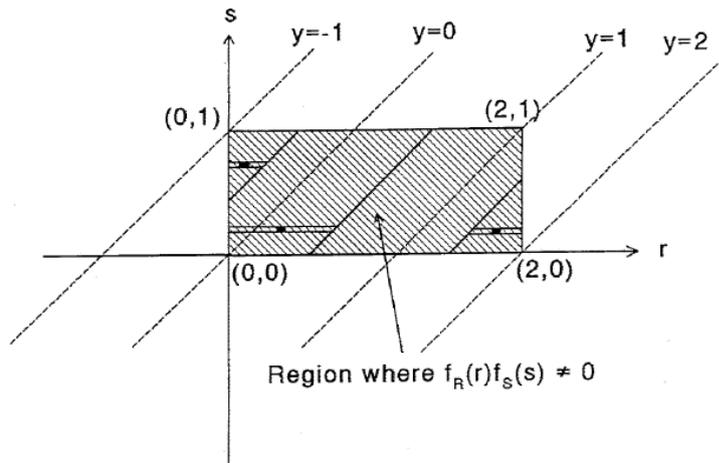
(d) $F_Z(1)$

(e) Explain why $F_Y(0) = F_Z(1)$

Solution:

(a) CDF of $Y = R - S$

$$F_Y(y) = P(Y \leq y) = P(R - S \leq y) = P(R - S - y \leq 0) = \iint_{R=\{r-s-y \leq 0\}} f_R(r)f_S(s)drds$$



For $-1 < y < 0$

$$F_Y(y) = \int_{-y}^1 \int_0^{s+y} \frac{1}{2}(2s)drds = \int_{-y}^1 s(s+y)ds = \left[\frac{s^3}{3} + y\frac{s^2}{2} \right]_{-y}^1 = \frac{1}{3} + \frac{y}{2} - \frac{y^3}{6}$$

For $0 < y < 1$

$$F_Y(y) = \int_0^1 \int_0^{s+y} \frac{1}{2}(2s)drds = \int_0^1 s(s+y)ds = \left[\frac{s^3}{3} + y\frac{s^2}{2} \right]_0^1 = \frac{1}{3} + \frac{y}{2}$$

For $1 < y < 2$

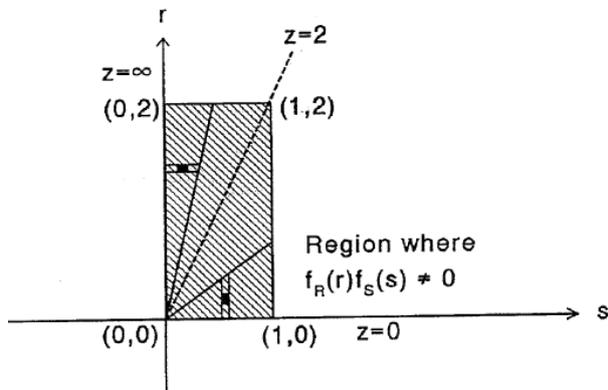
$$F_Y(y) = 1 - \int_0^{2-y} \int_{s+y}^2 \frac{1}{2}(2s)drds = 1 - \int_0^{2-y} s(2-s-y)ds = 1 - \left[s^2 - \frac{s^3}{3} - y\frac{s^2}{2} \right]_0^{2-y} = 1 - \frac{(2-y)^3}{6}$$

Therefore

$$F_Y(y) = \begin{cases} 0 & y \leq -1 \\ \frac{1}{3} + \frac{y}{2} - \frac{y^3}{6} & -1 \leq y \leq 0 \\ \frac{1}{3} + \frac{y}{2} & 0 \leq y \leq 1 \\ 1 - \frac{(2-y)^3}{6} & 1 \leq y \leq 2 \\ 1 & 2 \leq y \end{cases}$$

(a) CDF of $Z = R/S$

$$F_Y(y) = P(Z \leq z) = P\left(\frac{R}{S} - z \leq 0\right) = \iint_{R=\{r/s-z \leq 0\}} f_R(r)f_S(s)drds$$



For $0 < z < 2$

$$F_Z(z) = \int_0^1 \int_0^{sz} \frac{1}{2} (2s) dr ds = \int_0^1 s^2 z ds = \left[z \frac{s^3}{3} \right]_0^1 = \frac{z}{3}$$

For $z > 2$

$$F_Z(z) = 1 - \int_0^{2/z} \int_0^{r/z} \frac{1}{2} (2s) ds dr = 1 - \frac{1}{2} \int_0^{2/z} \frac{r^2}{z^2} dr = 1 - \frac{1}{2z^2} \left[\frac{r^3}{3} \right]_0^{2/z} = 1 - \frac{4}{3z^2}$$

Therefore

$$F_Z(z) = \begin{cases} 0 & z \leq 0 \\ \frac{z}{3} & 0 \leq z \leq 2 \\ 1 - \frac{4}{3z^2} & z \geq 2 \end{cases}$$

$$(c) F_Y(0) = \frac{1}{3} + \frac{0}{2} = \frac{1}{3}$$

$$(d) F_Z(1) = \frac{1}{3}$$

$$(e) F_Y(0) = P(Y \leq 0) = P(R - S \leq 0) = P(R/S - 1 \leq 0) = P(Z \leq 1) = F_Z(1)$$

Both probabilities represent the probability of event when $R < S$; i.e., when the applied load exceeds the resistance of the mechanical component. Since this is a failure event for this component, this probability is called the probability of failure.